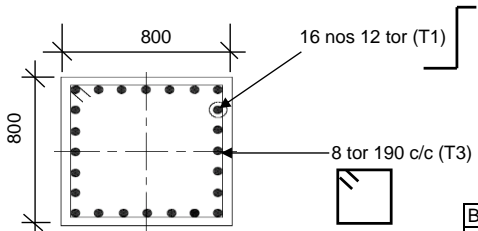


**BEFORE CASTING THE FOUNDATION VERIFY THE DIMENSIONS OF THE FOUNDATION BOLT (DIA.& QTY.) AND ANCHOR PLATE (PCD) WITH RESPECT TO THE DIMENSIONS MENTIONED IN THIS DRG.**

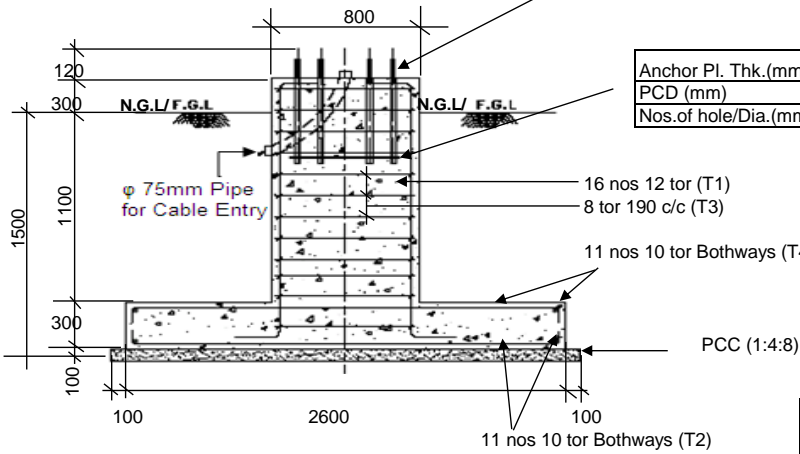
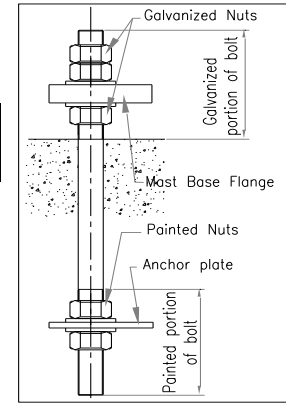
**FOUNDATION LOADINGS**

WIND SPEED	(M/SEC)	50.0
BENDING MOMENT	(T-M)	5.87
HORIZONTAL SHEAR	(T)	0.78
VERTICAL LOAD	(T)	0.66
MAX GR BEARING PRESSURE	(T/M <sup>2</sup> )	5.23
SAFETY FACTOR AGAINST OVERTURNING		2.25
CONCRETE MIX VIBRATED		M-20
MIN COVER	(MM)	50
STEEL		Fe-500
SOIL BEARING CAPACITY	(T/M <sup>2</sup> )	40.79
GROUND WATER TABLE		1.5m



**DETAIL OF PEDESTAL**

Bolt Nos.	=	6
Bolt Dia.	=	24 mm
Length	=	850 mm

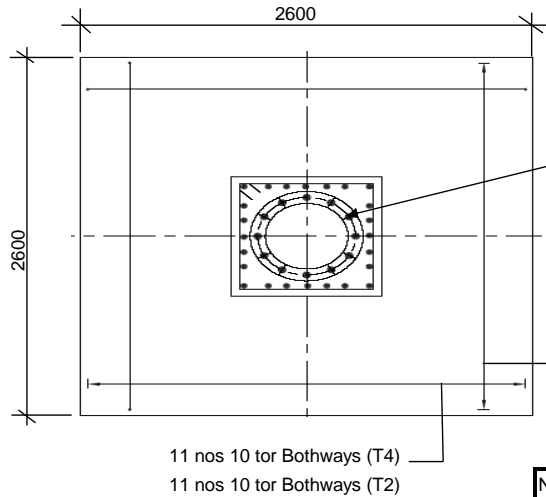


**SECTIONAL ELEVATION**

Anchor Pl. Thk.(mm)	=	6 mm
PCD (mm)	=	445 mm
Nos.of hole/Dia.(mm)	=	6 / 30

**BAR BENDING SCHEDULE**

MK	QTY	SIZE	LENGTH	SHAPE
T1	16	Φ 12	1995	100
T2	22	Φ 10	2700	100
T3	9	Φ 8	2992	700
T4	22	Φ 10	2700	100



**SECTIONAL PLAN**

**QUANTITIES**

RCC (M <sup>3</sup> )	PCC (M <sup>3</sup> )	STEEL (kg)
2.92	0.78	117.96

**NOTES**

- 1- ALL DIMENSIONS ARE IN MM. DO NOT SCALE THE DRAWING
- 2- MIN. LAP LENGTH OF BARS SHALL BE 50xD. UNLESS OTHERWISE STATED.
- 3- WE RECOMMENDED THAT MAST FLANGE REMAIN UNGROUTED
- 4- IF GROUTING IS CARRIED OUT IT IS ESSENTIAL TO LEAVE A MINIMUM OF 4 NOS 25MM DIA DUCTS EQUALLY SPACED AROUND THE FLANGE TO ALLOW DRAINAGE AND VENTILATION
- 5- BARS DRAWN IN THE DRAWING ARE FOR ILLUSTRATION ONLY. REFER TO THE NUMBERS SHOWN FOR ACTUAL REINFORCEMENT QUANTITY.

This drawing is the property of "BAJAJ ELECTRICALS LTD." & must be returned on request. It is submitted as confidential information in connection with enquiry, tender, orders or contracts. It is not to be used for any other purpose or order nor may it be copied or lent without our authority in writing

REV	DESCRIPTION	DATE

DATE	12/1/24	TITLE: General Arrangement Foundation Drawing for 16m High Mast
DRN BY	AUTO	
DSGD BY		
CHKD BY		
APPRD BY		
SCALE	NTS	M/S- PLATEFORMES INDUSTRIELLES DU CONGO POINTE-NOIRE SAU

Sheet No.	01 of 01	Rev.	0
DRAWING NUMBER: -			
EX000621-16M_HM(250W_12F)_PLATEFORMES INDUSTRIELLES_R0_SK			

**FOUNDATION DESIGN CALCULATIONS OF 16 M HIGH MAST  
M/S- PLATEFORMES INDUSTRIELLES DU CONGO POINTE-NOIRE SAU  
Republic of the Congo - Soil investigation Part 02 (20221223 - 20230201)**

**A. DESIGN PARAMETERS**

1)	Soil Bearing Capacity	:	40.79 T/m <sup>2</sup> as per SBC report
2)	Ground Water Table	:	1.5m
3)	Grade of concrete	:	M- 20

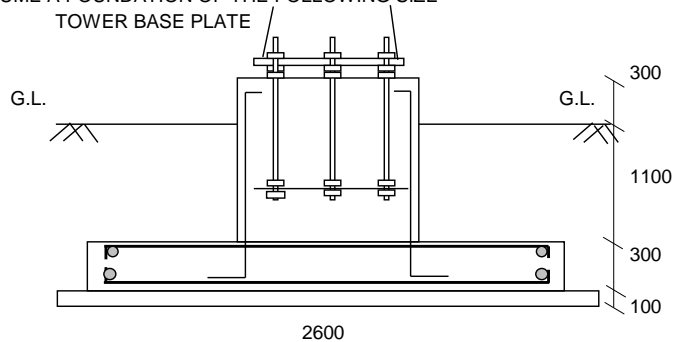
**B LOADS AT BOTTOM OF MAST AS PER ULTIMATE LIMIT STATE**

1)	Max.wind pressure (Wp) $Wp = 0.06 \times Vd \times Vd$	:	1349.76 N/m <sup>2</sup>
2)	Total wind force on luminaire (Wfl) $Wfl = Awt \times Wp$	:	1188.47 N
3)	Unit wind pressure at the top of the mast (Wt) = $Sf \times d \times Wp$	:	149.62 N/m.
4)	Unit wind pressure at the bottom of the mast (WB) = $Sf \times D \times Wp$	:	359.09 N/m.
5)	Net wind pressure on complete mast $(Wnet) = ((Wt + Wb)/2) \times Ht$	:	4069.70 N
6)	Total horizontal force on complete mast	:	7.64 kN
7)	Over turning moment at base of the mast	:	73.04 kN-m

Thus various forces acting on the foundation are as follows

1)	Downward/ Vertical load of the mast system (Fv)	:	656.00 kg 0.66 T
2)	Total horizontal force	:	778.56 kg
3)	Moment at the base of the foundation $(73.04 + 7.64 \times (1.4 + 0.3)) / 1.24 \times 100$	:	7045.25 kg-m

ASSUME A FOUNDATION OF THE FOLLOWING SIZE  
TOWER BASE PLATE



Size of Pedestal (L1,B1)	=	0.80 m
Height of pedestal (H1)	=	1.40 m
Height of pedestal above ground level(h1)	=	0.30 m
Size of raft (L2,B2)	=	2.60 m
Thickness of raft (H2)	=	0.30 m
depth of foundation above PCC & below FGL	=	1.40 m

Check for Soil pressure

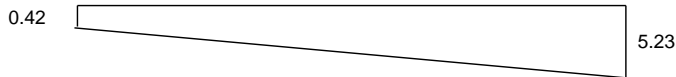
Density of Concrete	=	2.50 T/m <sup>3</sup>
<u>Weight of foundation (Wf)</u>		
= Weight of pedestal + Weight of raft	=	7.31 T
Density of soil	=	1.65 T/m <sup>3</sup>
		as per SBC report
<u>Weight of soil acting on raft (Ws)</u>	=	11.11 T

Thus total vertical load acting on the soil below foundation is  
F<sub>v</sub> = Weight of system + weight of foundation + weight of soil

$$= F_v + W_f + W_s = 19.07 \text{ T}$$

The Design verification for safe bearing pressure as follows.

Section modulus Z	=	$L^2 \times B^2 / 6$
Z	=	2.93 m <sup>3</sup>
Soil pressure	=	$[(P / L \times B^2) \pm (M/Z)]$
Pmax	=	5.23 T/m <sup>2</sup>
Pmin	=	0.42 T/m <sup>2</sup>
e (M/P)	=	0.37 m
B $3(B/2 - e)$	=	2.79 m
% of Foundation in contact with ground (Under submerged condition)	=	95.20 %
	=	5.23 T/m <sup>2</sup>
		< 40.79 <b>SAFE</b>



Check against overturning

Factor of safety = Restoring moment(due to D.L ) / Over turningmoment

$$\begin{aligned} \text{Restoring moment for 50 \% of soil weight} &= F_2 \times L^2 / 2 \times 0.9 \\ &= 15.82 \text{ T-m} \end{aligned}$$

$$\begin{aligned} \text{Factor of safety} &= 2.25 \\ &> 1.50 \quad \text{SAFE} \end{aligned}$$

Check against sliding

Sliding force	=	0.7786 T	
Coefficient of friction ( tan 25 )	=	0.466	
Frictional capacity	=	8.89 T	
Factor of safety	=	11.42	
		> 1.50	<b>SAFE</b>

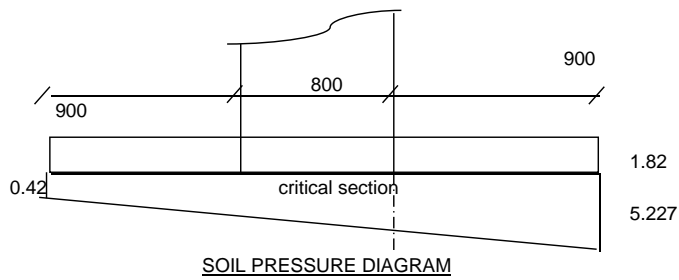
DESIGN OF PEDESTAL

Pedestal size	=	800X800 mm
Check for L/D	=	1.88
Design as Pedestal		
Load on pedestal -P	=	2.90 T
Moment @ bottom of pedestal -M	=	8.536 T-m
Assume Cover	=	50 mm
Pu / fck bd	=	0.0036
Mu / fck bd <sup>2</sup>	=	0.0145
d' /D Refer design aids of concrete, Chart 44	=	0.06
p / fck	=	negligible
pt (Provide a min of 0.15% steel.)	=	negligible %
Consider diameter of bar	=	12 mm
Assume Pt	=	0.27 %
Nos of Bar Required	=	16
pt <sub>ACT</sub>	=	0.3 %
8 Tor Rings at c/c of	=	190 c/c

**Provide 16 tor 12 mm steel as longitudinal reinforcement & tor 8 mm ties @ 190 c/c.**

Z of pedestal = 1/6 * B <sup>3</sup>	=	8.5E+07 m <sup>3</sup>	
Direct Stress Due to P (P/A) s <sub>cc,cal</sub>	=	0.07 N/m <sup>2</sup>	
s <sub>cc</sub>		< 5	<b>SAFE</b>
Bending Stress due to M (M/Z) s <sub>cbc,cal</sub>	=	1.500 N/m <sup>2</sup>	
s <sub>cbc</sub>		< 7	<b>SAFE</b>
Combined Stress (s <sub>cc,cal</sub> / s <sub>cc</sub> + s <sub>cbc,cal</sub> / s <sub>cbc</sub> )	=	0.23 N/m <sup>2</sup>	
		< 1	<b>SAFE</b>

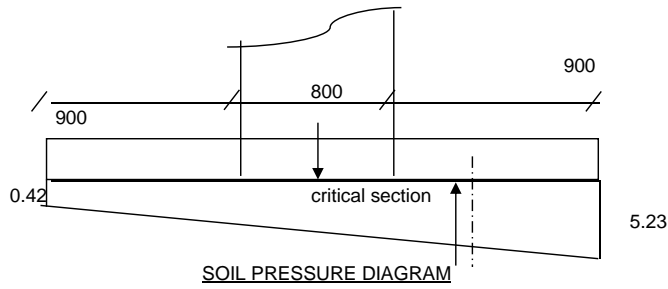
DESIGN OF RAFT



Effective cantilever span	=	0.9 m
Soil Pressure @ critical section	=	3.56 T/m <sup>2</sup>
Net Max. Cantilever moment @ bottom	=	1.16 T-m/m
$3.56 \times 0.9^2/2 + 0.5 \times (5.23 - 3.562) \times 0.9 \times 0.9^2/3 - 1.82 \times 0.9^2/2$		
Mu	=	17.35 kN-m/m
Assume Cover	=	50 mm
d 300-50-10/2	=	245 mm
Mu / bd <sup>2</sup>	=	0.289
Pt	=	0.087 %
Pt act	=	0.141 %
Ast/m (Provide Ptmin=0.12%)	=	294 mm <sup>2</sup>
Consider diameter of bar	=	10 mm
Spacing of bars	=	250 mm
<u>11 tor 10 bothways @ bottom</u>		
Soil Pressure from top	=	1.82 T/m <sup>2</sup>
Max. Cantilever moment on top	=	0.37 T-m/m
Mu at top	=	5.51 kN-m/m
Mu / bd <sup>2</sup>	=	0.092
Pt	=	0.028 %
Pt act	=	0.141 %
<u>Ast/m (Provide Ptmin=0.12%)</u>	=	360 mm <sup>2</sup>
Consider diameter of bar	=	10 mm
Spacing of bars	=	250 mm
<u>11 tor 10 bothways @ top</u>		

CHECK FOR ONE WAY SHEAR

Critical section is at 'd ' from face of column.

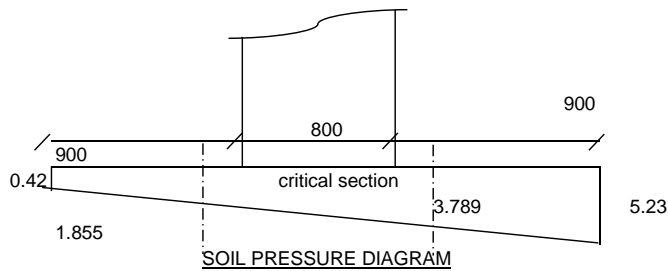


Distance of critical section for one way shear from edge	=	0.655 m
Soil Pressure at the critical section	=	4.01 T/m <sup>2</sup>
Max. shear force	=	3.03 T/m
Factored shear force	=	45.40 kN/m
Shear stress	=	0.185 N/mm <sup>2</sup>
b	=	16.464
Permissible shear stress	=	0.280 N/mm <sup>2</sup>

**SAFE**

CHECK FOR TWO WAY SHEAR

Critical section is at 'd/2 ' from face of column.



Distance of critical section for two way shear from edge	=	0.7775 m
Soil Pressure at the critical section	=	3.79 T/m <sup>2</sup>
Max. shear force	=	15.99 T
Factored shear force	=	239.88 kN
B0	=	1045.00 mm
Shear stress	=	0.23 N/mm <sup>2</sup>
Permissible shear stress	=	$k_s \sqrt{T_c}$
	=	$0.25 \times 20^{0.5}$
	=	1.12 N/mm <sup>2</sup>

**SAFE**